SOLANO			Solano C	County	675 Texas Street Fairfield, California 94533 www.solanocounty.com
COUNTY			Agenda Su	ubmittal	
Agenda #:		2	Status:	ALUC-Regular-NW	
Туре:		ALUC-Document	Department:	Airport Land Use Commissi	on
File #:		AC 20-003	Contact:	Jim Leland 707784-6765	
Agenda date:		1/9/2020	Final action:		
Title:		ALUC-19-18 (Benicia Conduct a Public Hea with the Travis Air For	a Solar Project) ring to consider a ce Base Land U	a Consistency Determination for th se Compatibility Plan (County of S	ne Benicia Solar Project olano)
Governing body:	:	Airport Land Use Com	mission		
District:					
Attachments:		A Application			
		A1 Project Description	<u>1</u>		
		A2 Vicinity Map			
		A3 Aerial Map			
		<u>A4 Plans</u>			
		A5 SGHAT Analysis			
		A6 Proposed Zoning	Text Amendmen	<u>t</u>	
		B Travis Context Map	Map		
Date	Ver.	Action By		Action	Result

Published Notice Required?	Yes	No	
Public Hearing Required?	Yes _	No	

DISCUSSION:

INTRODUCTION

The City of Benicia is considering a proposal to establish a commercial scale solar electric generation project on the north side of Lake Herman Road opposite the intersection with Reservoir Road (See Attachment A1 Project Description). The project site is approximately 90 acres in size and is located within Compatibility Zone D of the Travis Plan.

According to the project description, the project will:

"..... generate a total of 5.0 Megawatts (MW) AC (7 MW DC) of clean, reliable solar energy when complete. The Project will interconnect to PG&E's pre-existing electrical distribution system located on site. The power generated from this facility will be sold to Marin Clean Energy (MCE) through a long-term Power Purchase Agreement (PPA). Additionally, the Project will be equipped with energy storage technology that will allow on site renewable energy generation to be stored and dispatched onto the grid when needed.

The Lake Herman Solar Project will utilize approximately 18,424 solar modules and 40 string inverters, which

convert the sun's energy into usable, AC power. Single axis tracking technology will be utilized to allow the modules to efficiently track the sun throughout the day and maximize the efficiency of solar collection. The modules will be mounted on a steel racking system, which will be anchored into the ground using driven steel piers. The overall height of the array will be no more than 8 feet tall."

The project will be located on property in the City of Benicia with an open space zoning designation. As a part of the process, the City will be considering a zoning text amendment which would allow commercial scale solar projects within the open space zoning district with a use permit. (See Attachment A6 Proposed Zoning Text Amendment).

REQUIRED TESTS FOR CONSISTENCY

ALUC Review Requirements

State law, under Section 21661.5 of the Public Utilities Code, requires that any proposed zoning regulations or revisions to the local zoning ordinance be reviewed for consistency with adopted airport land use compatibility plans.

The ALUC is concerned with those aspects of the proposed zoning changes which have the potential to be incompatible with of the Travis Air Force Base Land Use Compatibility Plan.

California Airport Land Use Planning Handbook

The State Department of Aeronautics has published the California Airport Land Use Planning Handbook as a guide for Airport Land Use Commissions in the preparation and implementation of Land Use Compatibility Plans and Procedure Documents. Section 6.4.2 sets forth procedures for the review of local zoning ordinances and directs agencies to consider the topics listed in Table 5A, as follows:

Zoning or Other Policy Documents (from Table 5A, CalTRANS Airport Land Use Planning Handbook)

The Handbook lists the following topics for consideration when reviewing zoning or other policy documents.

- Intensity Limitations on Nonresidential Uses
- Identification of Prohibited Uses
- Open Land Requirements
- Infill Development
- Height Limitations and Other Hazards to Flight
- Buyer Awareness Measures
- Non-conforming Uses and Reconstruction

Staff has reviewed the Benicia Solar Project in light of the tests outlined above as well as the specific compatibility factors applicable to lands within the City of Benicia. Our analysis is presented below.

ALUC Context

The Benicia Solar Project applies to properties which lie within the area of influence of the Travis AFB Land Use Compatibility Plan (Travis Plan), more particularly within Compatibility Zone D (See Attachments B, C and D).

Travis Air Force Base Land Use Compatibility Plan

The requirements for Compatibility Zone D are listed below under the appropriate topical areas from topics suggested for

File #: AC 20-003, Version: 1

consideration as identified in the State Handbook. They are as follows:

- Intensity Limitations None
- Identification of Prohibited Uses Hazards to Flight (See below)
- Open Land Requirements None
- Infill Development Not Applicable
- Height Limitations and Other Hazards to Flight
 - ALUC review required for objects > 200 feet AGL
 - All proposed wind turbines must meet line-of-sight criteria in Policy 3.3.4
 - All new or expanded commercial-scale solar facilities must conduct an SGHAT glint and glare study for ALUC review
 - All new or expanded meteorological towers > 200 feet AGL, whether temporary or permanent, require ALUC review
 - Areas within the Bird Strike Hazard Zone must prepare a WHA and incorporate all feasible mitigation measures.
 - Outside of the Bird Strike Hazard Zone but within the Outer Perimeter, any new or expanded land use that has the potential to attract the movement of wildlife that could cause bird strikes are required to prepare a WHA.
- Buyer Awareness Measures None
- Non-conforming Uses and Reconstruction Not Applicable

Staff has reviewed the proposed Benicia Solar Project Ordinance for consistency with the compatibility criteria for Compatibility Zone D of the Travis Plan. Our analysis is presented below.

ANALYSIS

Intensity Limitations on Nonresidential Uses

Within Compatibility Zone D, there are no limitations on intensity for non-residential land uses and as a result the Benicia Solar Project is consistent with this provision.

Identification of Prohibited Uses

There are no prohibited uses within Compatibility Zone D. Therefore, the Benicia Solar Project is consistent with this provision.

Open Land Requirements

Compatibility Zone D has no open land requirements for development. As a result, the Benicia Solar Project is consistent with this requirement.

Infill Development

This project is not a part of an infill development. No further consideration is required for this criterion.

Height Limitations and Other Hazards to Flight

The "Height Limitations" and "Other Development Conditions" listed in Compatibility Zone D are as follows:

- 1. ALUC review required for objects > 200 feet AGL
- 2. All proposed wind turbines in excess of 100 feet in height must meet line-of-sight criteria in Policy 3.4.4
- 3. All new or expanded commercial-scale solar facilities must conduct an SGHAT glint and glare study for ALUC review
- 4. All new or expanded meteorological towers > 200 feet AGL, whether temporary or permanent, require ALUC review
- 5. For areas within the Bird Strike Hazard Zone, reviewing agencies shall prepare a WHA for discretionary projects that have the potential to attract wildlife that could cause bird strikes. Based on the findings of the WHA, all reasonably feasible mitigation measures must be incorporated into the planned land use.
- 6. For areas outside of the Bird Strike Hazard Zone but within the Outer Perimeter, any new or expanded land use involving discretionary review that has the potential to attract the movement of wildlife that could cause bird strikes are required to prepare a WHA.

None of the hazards listed above are associated with the lawful use of the property for cannabis business purposes for reasons discussed in the following sections.

1 & 4. Height Review for Objects Greater than 200 Feet in Height

The Benicia Solar Project do not permit any structures taller than 50 feet, so ALUC review of this item is not required.

2. Wind Turbines in Excess of 100 Feet in Height

The Benicia Solar Project do not permit any wind turbines, so ALUC review of this item is not required.

3. Commercial Scale Solar Projects

Commercial Solar projects require review by the Airport Land Use Commission. The Travis Plan requires that commercial solar projects submit a SGHAT analysis for review by the ALUC (See Attachment A5). The Solar Glare Hazard Analysis indicates that there will be no adverse impact to Travis AFB by the installation and operation of the proposed solar project. As such, the Benicia Solar Project is consistent with this provision.

5 & 6 Projects within the Bird Strike Hazard Zone or the Outer Perimeter Area

The solar project lies outside of the Bird Strike Hazard Zone and the Outer Perimeter Area. As a result, the Benicia Solar Project is not subject to the bird strike requirements within the Travis Plan.

Buyer Awareness Measures

The proposed project lies within Compatibility Zone D and outside of any noise contours of concern. As a result, Buyer Awareness Measures are not required by the Travis Plan.

Non-conforming Uses and Reconstruction

The project is proposed on vacant land and does not require review under the non-conforming provisions.

CONCLUSION

The analysis above, including the SGHAT, demonstrates that the specific solar project being proposed is consistent with the Travis Plan. The zoning text amendment could permit other solar facilities on other open space lands. Staff is recommending that the solar standards proposed in the zoning text amendment be revised to include the following language:

" All solar utility projects shall prepare a solar glare analysis utilizing a SGHAT compliant analytical tool. Solar utility projects, including the results of the SGHAT analysis, shall be submitted to the Solano County Airport Land Use Commission for a consistency determination prior to approval by the City."

This provision would reflect the requirements of the Travis Plan which apply to new solar projects being considered by local jurisdictions.

RECOMMENDATION

Adopt the recommended findings and determine that the Benicia Solar Project, including the recommended additional language from above, is **consistent** with the Travis Air Force Base Land Use Compatibility Plan.

Attachments

File #: AC 20-003, Version: 1

- Attachment A: Application
- Attachment A1 Application Project Description
- Attachment A2 Vicinity Map
- Attachment A3 Aerial Map
- Attachment A4 Plans
- Attachment A5 SGHAT Analysis
- Attachment A6 Proposed Zoning Text Amendment
- Attachment B: Travis Plan Context Map
- Attachment C: Resolution (To be Distributed at Hearing)

Solano County Airport Land Use Commission

675 Texas Street Suite 5500 Fairfield, CA 94533 Tel 707.784.6765 Fax 707.784.4805

LAND USE COMPATIBILITY DETERMINATION: APPLICATION FORM

TO BE COI	MPLETED BY STAFF	
APPLICATION NUMBER:	FILING FEE:	
DATE FILED:	RECEIPT NUMBER:	
JURISDICTION:	RECEIVED BY:	
PROJECT APN(S):		
TO BE COMPLE	TED BY THE APPLIC	ANT
I. GENEF	RAL INFORMATION	
NAME OF AGENCY:		DATE:
City of Benicia		December 5, 2019
ADDRESS:		
250 East L Street, Benicia, CA 94510		
E-MAIL ADDRESS: sthorsen@ci.benicia.ca.us	DAYTIME PHONE: (707) 746-4382	FAX: (707) 747-1637
NAME OF PROPERTY OWNER:		DATE:
Benicia North Gateway, LLC		
ADDRESS:		DAYTIME PHONE:
Attn: Bradley Lowe 4171 Essen Lane, Baton Rouge, LA 7080	9	(225) 932-5884
NAME OF DOCUMENT PREPARER:		DATE:
Suzanne Thorsen, City of Benicia		December 5, 2019
ADDRESS:	DAYTIME PHONE:	FAX:
250 East L Street, Benicia CA 94510	(707) 746-4382	(707) 747-1637
NAME OF PROJECT:		
Lake Herman Solar Facility		
PROJECT LOCATION:		
88.54 acre parcel located on north side of La Open Space (OS) within City of Benicia APN	ike Herman Road, zoned I 0080-030-050	
STREET ADDRESS:		
No address		

PLEASE CALL THE APPOINTMENT DESK AT (707) 784-6765 FOR AN APPLICATION APPOINTMENT.

LAND USE COMPATIBILITY DETERMINATION APPLICATION

TO BE COMPLETED BY THE APPLICANT

II. DESCRIPTION OF PROJECT

Development of five Megawatt (MW) AC solar farm - please see attached documentation and written description. Project requires City of Benicia approval of zoning text amendment to establish new use classification in OS District (solar utility); adoption of IS/MND and Mitigation Monitoring and Reporting Program; use permit and design review. No grading permit nor extension of urban utilities is required.

PLEASE CALL THE APPOINTMENT DESK AT (707) 784-6765 FOR AN APPLICATION APPOINTMENT.

Page 3

LAND USE COMPATIBILITY DETERMINATION APPLICATION

TO BE COMPLETED	BY THE APPLICANT
II. DESCRIPTION OF	PROJECT (CONT'D)
POTENTIAL PROJECT EMISSIONS: (i.e. smoke, stean None	η, glare, radio, signals):
PROJECT AIRPORT LAND USE COMPATIBILITY PLAN: Travis Airport Land Use Compatibility Plan	COMPATIBILITY ZONE: D
PERCENTAGE OF LAND COVERAGE:	MAXIMUM PERSONS PER ACRE: 0
40% lot coverage	
 THE FOLLOWING INFORMATION MUST BE SUBMITT JURISDICTION REFERRAL LETTER: ENVIRONMENTAL DOCUMENTATION: LOCATION MAP: ASSESSOR'S PARCEL MAP, with subject property SITE PLAN, drawn to scale and fully dimensioned in reduction(s): ELEVATIONS, if located in APZ, clear zones and A x 11 inch reduction(s) : WIND TURBINE STUDY, including cumulative impathe individual effects of the proposed project, and (2) the proposed project considered in connection with the projects and proposed projects, and the effects of p for wind energy development of the remaining vacant Solano County General Plan and (ii) any probable report structures having different dimensions. SUPPLEMENTAL INFORMATION: FEES: ELECTRONIC COPIES OF ALL APPLICATION MA 	ED AS A MINIMUM REQUIREMENT: "marked in red: ncluding topographical information, and 8 1/2 x 11 inch ,B,C compatibility zones or over 200' in height, plus 8 1/2 act studies. Such studies shall include an analysis of (1) as required by law, an analysis of the cumulative effects of ne effects of past projects, the effects of other current robable future projects, including (i) the probable build out parcels within the wind resource areas described in the blacement of existing turbines or meteorological towers with TTERIALS ONA CD: Provided on flash drive
APPLICANT SIGNATURE:	DATE:
DOES THE PROJECT PROPOSE THE DEMOLITION O ON THE PROJECT SITE? YES NO If yes	DR ALTERATION OF ANY EXISTING STRUCTURES , describe below:

PLEASE CALL THE APPOINTMENT DESK AT (707) 784-6765 FOR AN APPLICATION APPOINTMENT.



July 12, 2019

Suzanne Thorsen Principal Planner Community Development Department 250 East L Street Benicia, CA 94510

Dear Suzanne,

RE: Lake Herman Solar Project – Written Statement

In accordance with Use Permit and Design Review Submission, please find an updated description of the proposed project below:

The Lake Herman Solar project ("Project") is a small-scale utility solar and energy storage project located on approximately 35 acres of an 89-acre parcel of land in the City of Benicia, CA. The Project is located off Lake Herman Road (APN # 0080-030-050). Renewable Properties, LLC has entered into a purchase agreement with the property owner (Benicia North Gateway II, LLC) to facilitate the development of a small scale, utility solar power generation facility.

The Project will generate a total of 5.0 Megawatts (MW) AC (7 MW DC) of clean, reliable solar energy when complete. The Project will interconnect to PG&E's pre-existing electrical distribution system located on site. The power generated from this facility will be sold to Marin Clean Energy (MCE) through a long-term Power Purchase Agreement (PPA). Additionally, the Project will be equipped with energy storage technology that will allow on site renewable energy generation to be stored and dispatched onto the grid when needed.

The Lake Herman Solar Project will utilize approximately 18,424 solar modules and 40 string inverters, which convert the sun's energy into usable, AC power. Single axis tracking technology will be utilized to allow the modules to efficiently track the sun throughout the day and maximize the efficiency of solar collection. The modules will be mounted on a steel racking system, which will be anchored into the ground using driven steel piers. The overall height of the array will be no more than 8 feet tall.

Please don't hesitate to reach out with any questions or comments. We look forward to working with you to bring this project to fruition.

Sincerely

Aaron Halimi President

Attachment B: Vicinity Map



Attachment C: Aerial Map





1

ARRAY PLAN SCALE:1"=100'



	LEGEND
	ATI 84 MODULE TRACKER ROW
	ATI 56 MODULE TRACKER ROW
	POWER STATION (TYP.OF 2) - (1) MV TRANSFORMER, (1) DAS, (1) WEATHER STATION EQUIPMENT RACK (TYP. OF 10)- (4) SUNGROW 125kW STRING INVERTER (1) 600A MI O PANEL
<u>150202020</u>	20' WIDE SITE ACCESS GRAVEL ROAD
	12' WIDE PERIMETER DIRT ROAD
	(E) WETLAND
	PUBLIC ROAD
	HIGH SLOPE AREAS
	UNEVEN SLOPE AREAS
	VEGETATIVE SCREEN
	PROPERTY LINE
——————————————————————————————————————	PROPERTY LINE
	SETBACK
OVE	(E) OH LINES
——— ОНМУ ————	OVERHEAD MV CABLE
UGMV	UNDERGROUND MV CABLE
	GENERAL NOTES

1. REFER TO SINGLE LINE DIAGRAM FOR DETAILS.

- 2. INSTALLATION TO COMPLY WITH NEC 2014 ARTICLE 690 AND ALL APPLICABLE LOCAL, STATE AND NATIONAL CODES OR REGULATIONS.
- 3. EQUIPMENT SHALL BE LABELED PER NEC 690 AND UTILITY REGULATIONS.
- 4. 20' ACCESS ROADS SHALL BE DESIGNED TO ACCOMMODATE ALL CONSTRUCTION, OPERATIONS, MAINTENANCE, AND UTILITY TRAFFIC THROUGHOUT THE SITE.
- 5. DIMENSIONS TO PROPERTY LINES AND EXISTING FEATURES ARE APPROXIMATE PENDING SURVEY.
- 6. THE CROSS SECTION OF THE PROPOSED 10 FT WIDE ROAD WILL MATCH THE EXISTING GRADE, WHICH SLOPES TOWARD THE PERIMETER FENCE. ROAD CROSS SECTIONS WILL BE DESIGNED TO DRAIN TOWARDS THE FENCE. FINAL CIVIL DESIGN WILL SPECIFY THE PROPOSED GRADES.
- 7. ALL DRIVE AISLES WILL COMPLY WITH BMC CHAPTER 17.74.







TYPICAL INTERNAL ACCESS GRAVEL ROAD CROSS SECTION (NOTE 6)

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SCALE:NTS

GRAVEL ROAD CROSS SECTION



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drawing no.: PV-100
DRAWN BY:
LR
REVIEWED BY:
DATE:
09/17/19
SCALE:
AS SHOWN
PROJECT NO .:



	LEGEND
	ATI 84 MODULE TRACKER ROW
	ATI 56 MODULE TRACKER ROW
	POWER STATION (TYP.OF 2) - (1) MV TRANSFORMER, (1) DAS, (1) WEATHER STATION
	EQUIPMENT RACK (TYP. OF 10)- (4) SUNGROW 125kW STRING INVERTER, (1) 600A MLO PANEL
<u>\$0\$0\$(</u>	20' WIDE SITE ACCESS GRAVEL ROAD
	12' WIDE PERIMETER DIRT ROAD
	(E) WETLAND
	PUBLIC ROAD
	HIGH SLOPE AREAS
	UNEVEN SLOPE AREAS
	VEGETATIVE SCREEN
- ·	PROPERTY LINE
Х	PROPERTY LINE
	SETBACK
• OVE	(E) OH LINES
онму ———	OVERHEAD MV CABLE
UGMV	UNDERGROUND MV CABLE



FOR UTILITY APPLICATION	09/18/19
DESCRIPTION	DATE
	FOR UTILITY APPLICATION DESCRIPTION

SHEET TITLE:

CIRCULATION PLAN FOR VEHICLES

drawing no.: PV-101
DRAWN BY:
REVIEWED BY:
DATE: 09/17/19
SCALE:
AS SHOWN



RENEWABLE PROPERTIES LAKE HERMAN SOLAR LAKE HERMAN RD, BENICIA, CA 94510, USA LAT: 38.097075° LON: -122.141678° 0 FOR UTILITY APPLICATION 09/18/19 DATE REV. NO DESCRIPTION SHEET TITLE: INTERCONNECTION DETAILS DRAWING NO.: PV-102 DRAWN BY: LR REVIEWED BY: DATE: 09/17/19 SCALE: AS SHOWN

SCALE: NTS

PROJECT NO .:

Glare Impact Study of Lake Herman Solar Facility



Thomas Cleveland, PE Raleigh, NC July 29, 2019

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Executive Summary

Photovoltaic (PV) modules (aka solar panels) are designed to absorb, and thus not reflect, close to 100% of the solar energy that strikes them. However, when sunlight strikes the glass front of a solar panel at a glancing angle a significant portion of the solar radiation is reflected, which can potentially lead to solar glint or glare impacting a person's vision, including pilots landing aircraft. Thankfully, the conditions required for a PV project to create hazardous glare rarely occur. Also, it is possible to use specialized 3-D modeling software to predict when and where glare may be produced, which allows adjustment of solar project designs before they are constructed in order to avoid the potential for glare hazards.

To avoid construction of solar PV projects that could create a solar glare hazard for aircraft, the Federal Aviation Administration (FAA) and the US Department of Energy's Sandia National Laboratories partnered to develop a software to calculate the potential for a PV project to create glare intense enough to be a hazard to nearby aviation. The software, called Solar Glare Hazard Analysis Tool (SGHAT), may also be used to assess the potential for a PV project to cause solar glare for other viewers, such as vehicle drivers on nearby roads and neighbors looking out of their windows.

The analysis presented in this report used a privately licensed version of the SGHAT software, called ForgeSolar, to conduct a detailed site-specific PV solar glare analysis of the proposed Lake Herman Solar project (Project). The software from ForgeSolar has been validated as effective for this type of solar glare analysis. The software analysis checks for the potential for low or high intensity solar glare for every minute of the year at many user-defined observation points and/or routes. Specifically, the

analysis of the Lake Herman Solar project included the final approach flight paths for the six runways at Travis Air Force Base, the air traffic control tower at Travis Air Force Base, the 2-mile section of Lake Herman Road immediately south of the PV project, and buildings within about 1 mile of the site (see figure to the right for locations as modeled in ForgeSolar).

The analysis predicts **no glare** of any intensity at any time during the year at any of the analyzed observation locations.



Observation Locations Analyzed in ForgeSolar: Flight Paths at Travis Air Force Base in upper right (red lines); Lake Herman Road 2-way route (aqua lines), and buildings (red OP# markers) [Cover image shows Lake Herman Road and building locations in detail]

Background

At the request of RPCA Solar 4, LLC, I conducted an analysis of the potential for solar glare impacts by the proposed 5 MW_{AC} Lake Herman solar facility located on the northern city limits of Benicia, California. The study analyzed the potential for glare impacts to drivers on Lake Herman Road, pilots approaching the runways at Travis Air Force Base, the air traffic control tower at Travis Air Force Base, and residential and commercial neighbors within one mile.

Glare Impact Analysis

Intense glare can create a visual hazard. Every experienced driver is familiar with the type of glare shown in the photo to the right that occurs when an auto driver is heading directly into the rising or setting sun. Similarly, airplane and helicopter pilots often fly in the direction of the sun and thus experience very intense glare directly from the sun itself. Pilots also experience glare from reflections off a variety of objects on the ground, such as metal roofs, bodies of water, and car windshields. Consequently, pilots fly with sunglasses and tinted visors to minimize this hazard. The reflected glare produced by these objects is not nearly as intense as direct sunlight. Like many



Figure 1: Glare coming directly from the Sun

other objects on or near the ground, reflections off solar panels (aka PV modules) can also cause glare visible to pilots. There is also the potential for solar panels on or very near the airport to cause distracting glare for air traffic controllers. Due to these potential hazards, the Federal Aviation Administration (FAA) and the US Department of Energy's Sandia National Laboratories collaborated to create an online software tool, known as the Solar Glare Hazard Analysis Tool, or SGHAT, to analyze solar photovoltaic projects for their potential to create hazardous solar glare. After multiple years of free public availability, access to the SGHAT tool was ended in 2017 and the SGHAT technology was licensed to a private company, ForgeSolar. ForgeSolar improved upon the original SGHAT technology and offers a private solar glare hazard analysis tool, which is the only such tool available today. The analysis presented in this report used the current professional ForgeSolar software.

The software calculates the potential for glare at each modeled observer (e.g approaching pilot, passing motorist, neighbor) for every minute of the year. The model knows the position of the sun each minute, assumes a cloud-free sky, and calculates the potential for glare from each section of the proposed solar facility. The software can calculate not only whether there is a possibility for glare each minute, but also the intensity of the glare. Thus, it can assess the degree of hazard any glare may present to pilots and motorists.

Modeling the Lake Herman Solar Facility

The models presented in this report use the default SGHAT values for model variables that are not site specific, such as the sun subtended angle of 9.3 milliradians and 0.017 meter eye focal length. All the model variables are visible in the ForgeSolar results reports included in the appendix of this report.

Figure 2 shows the location of the PV array in the ForgeSolar model. The array layout from a Lake Herman site plan containing satellite imagery was overlaid over the ForgeSolar software so that the PV array location in the model accurately represents the location of the array in the actual project. To be conservative the array in ForgeSolar extends all the way to the site's perimeter fence.



Figure 2. Lake Herman PV Array in ForgeSolar (blue area with numbered vertices) with Overlay of Lake Herman Site Plan Showing the Array Layout, Site Fence, and Satellite Imagery

The entire project uses single-axis tracking racking to mount the PV modules. As is typical for this type of PV module racking, the array at the Lake Herman site consists of 1-module-wide rows that are each oriented along a North-South line. This North-South line is also the axis of rotation of each row. The basic motion is that each row slowly rotates over the course of every day from a 60-degree tilt toward the east at sunrise to a 60-degree tilt toward the west by sunset. Around midday when the sun is at its highest position in the sky the rows of modules are horizontal, with each module facing straight up. The ForgeSolar analysis assumes that the rows remain tilted 60 degrees (from horizontal) to the west from the time of sunset each day until the time of sunrise the next day. In actuality the tracking system is likely to be more sophisticated and implement automatic backtracking, which means that near sunrise and sunset the rows will tilt less than the full 60 degrees in order to avoid each row partially shading the row behind it. Solar module electricity production is very sensitive to partial shading, so the system can produce more power by facing the modules a little more horizontal than otherwise optimal if it means avoiding one row shading another. This backtracking will increase the incidence angle of the sunlight on the modules which increases the reflectivity of the modules and thus the potential for glare impacts.

Unfortunately, the ForgeSolar software is not currently able to model automatic backtracking; however, additional ForgeSolar simulations were conducted to assess the glare impact of backtracking. Four additional systems were analyzed, two with the PV array facing west and with a fixed-tilt 45 degrees and 30 degrees from horizontal and another two facing east also with tilts of 45 and 30 degrees. The west-facing models represent a backtracked array near sunset and the east-facing models represent a backtracked array near sunset and the east-facing models represent a backtracked array near sunset.

For all SGHAT models in this report, the solar array is modeled at a height of 5 feet, representing a typical height for the center of each PV module. Models were also run with array heights of 2 feet and 8 feet, representing the bottom and top of the array, as recommended in the SGHAT user manual. The results of the 2-ft and 8-ft height models were the same as the model with a 5-foot array height, so for simplicity only the 5-foot array data is presented in this report.



Figure 3. Diagram of PV Module Racking from the Lake Herman Solar Site Plan, Including Minimum Height Above Grade for Horizontal and Extreme Angles of Rotation

It is vital to realize that the software does <u>not</u> take into account visual obstructions between the solar array and the observer. This includes both topographical barriers, such as a hill, and living or man-made barriers such as a forest or building. A comprehensive analysis of the visibility of the solar array from each observation route or point is not included in this report, although aerial 3D surface models clearly show that several of the nearby buildings and the air traffic control tower at Travis Air Force Bases have their view of the solar array, and thus any glare it may produce, blocked by elevated topography between the observation point and every part of the array. For simplicity no potential relevant observation points were omitted from the ForgeSolar analysis due to having no line of sight to the array; however, some potential residential observation points were omitted from the ForgeSolar analysis due to other building blocking their sight of the array and because other modeled observation points represent a closer observation point along the same line of sight.

Analysis of the Travis Air Force Base Airport (KSUU)

This analysis modeled the potential for glare hazards for Travis Air Force Base (KSUU), which is located about 14.1 miles northeast from the Lake Herman Solar project (measured from the threshold of the closest runway to the closest solar module). The Travis Air Force Base Land Use Compatibility Plan classifies all the land around the base as one of several impact zones (Zones A to E) depending on its potential to impact operations at the base with Zone A having the most potential for impact. The proposed site for the Lake Herman Solar project is in Zone D, which requires that any commercial-scale solar facility not create a glare hazard at the base. To comply the solar project must not create glare along any final approach path that is more intense than glare that has a "low potential for after-image". Travis Air Force Base has six runways, Runway 3L/21R, Runway 03R/21L, and a shorter assault strip Runway 32/212. Each set of runways share the same physical runway but represent approaches from opposite ends. The specifics of the typical approach for each runway were set based on FAA data for Travis Air Force Base¹. The airport also has an air traffic control tower located just to the northwest of the runways that was included in the solar glare analysis as Observation Point 20.



Figure 4. Location of Travis Air Force Base Airport in Relation to the Lake Herman Solar Project Site; 14.1 Miles Between Them Along the Red Line (Image is Oriented with North Toward the Top)

¹ Sourced from <u>https://maps.avnwx.com/airport/KSUU</u> which presents the current airport data provided by FAA (<u>https://aeronav.faa.gov/afd/20jun2019/sw_233_20JUN2019.pdf</u>) in a user-friendly format



Figure 5. Approach Flight Paths (Red Lines) to Travis Air Force Base's Six Runways and the Airports Air Traffic Control Tower ("20 – ATCT" slightly to the left of the center of the image), as Modeled in ForgeSolar

As specified in the Interim Policy for the FAA Review of Solar Energy System Projects on Federally Obligated Airports², the ForgeSolar software examines the last two miles of the landing approach to each runway. The analysis is limited to this portion of the flight path because severe glare during the final approach has the potential to create a hazard for the pilot, whereas severe glare earlier in the flight is generally a not hazard.

The SGHAT results for the Project were **no glare** of any intensity during any minute of the year for any of the flight paths and for the air traffic control tower. The four additional ForgeSolar models representing intelligent backtracking of the array near sunrise and sunset predicted **no glare** from a backtracking array.

² "Interim Policy for the FAA Review of Solar Energy System Projects on Federally Obligated Airports.", http://www.gpo.gov/fdsys/pkg/FR-2013-10-23/pdf/2013-24729.pdf

Analysis of Potential Glare Impacts to Nearby Motorists

The proposed project is just to the north of Lake Herman Road, which is a small rural roadway, and was analyzed in ForgeSolar for any potential glare impacts from the proposed solar facility. The other nearby roads are small private roads with very limited traffic volume and slow traffic speeds, so these roads were not included in the ForgeSolar glare analysis. There are some rolling hills in the area, but the proposed solar facility is generally at the same elevation as Lake Herman Road. The rolling hills block view of the solar project along several portions of the road but there is limited vegetation to block motorists' views of the solar modules where there is no hill to impede view. Therefore, there are sections of Lake Herman road where the proposed solar project will be visible within 45 degrees of the automobile's direction of travel. The following two images from a 3D model of the site in Google Earth use elevated views from above the area to provide a sense of the views of the site for both the eastbound and westbound motorists on Lake Herman Road. The yellow area seen in these images show the location of the site footprint within the project's perimeter fence.



Figure 6. View from Southeast of the Solar Site from an Elevated Viewpoint across Lake Herman Road. Lake Herman is Visible in the Upper Left Corner of the Image. The Yellow Area is the site footprint within the perimeter fence.



Figure 7. View Facing East from above Lake Herman Road to the West of the Solar Site from an Elevated Viewpoint

ForgeSolar provides a "route" type of observation location that is designed to model the potential for glare hazards along roads and other routes. One route was modeled in ForgeSolar as shown in Figure 8, which is analyzed by ForgeSolar as both an eastbound route and a westbound route. The route was modeled at 3.5 feet above the ground, to represent the height of a driver, per the American Association of State Highway and Transportation Officials (AASHTO) eye height of a driver of a passenger vehicle³. The software checks for glare from up to 50 degrees from the direction of travel. Studies of pilots have shown that glare from beyond 45 degrees from their direction of travel does not present any glare hazard, and it is reasonable to assume that the same holds true for motor vehicle drivers as well.

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³ A Policy on Geometric Design of Highways and Streets. American Association of State Highway and Transportation Officials, Washington, D. C., 2004 edition



Figure 8. Observation Route on Lake Herman Road (Aqua Line) as Modeled in ForgeSolar, Approximately 2 Miles End-to-End

The SGHAT results for the Project were **no glare** of any intensity during any minute of the year for motorists on Lake Herman Road. The four additional ForgeSolar models representing intelligent backtracking of the array near sunrise and sunset predicted **no glare** from a backtracking array for motorists on Lake Herman Road.

Analysis of Residential and Commercial Neighbors

There is only one occupied building closer than ½ mile from the proposed solar facility, which is a home about 1/10 of a mile to the northwest of the project. There are numerous residential, industrial, and commercial buildings between about ½ and 1 mile from the PV site. Twenty of these buildings were included in the ForgeSolar model (Observation Points 2 through 19, 21, and 22. Observation Point 20 is the air traffic control tower at Travis Air Force Base). There are additional buildings within a 1-mile radius of the solar facility, but these buildings are either unoccupied, have their view blocked by a building included in the analysis, or are represented by the analysis results of a nearby building included in the analysis. All but four of the buildings within 1 mile of the proposed site are in an area of development to the south of the project. Most of the buildings have their view of the Project at least partially blocked by higher ground between the building and the site, and some of the buildings have their view fully blocked by a hill. Rather than include a line-of-site to justify not modeling some buildings all appropriate buildings were simply included in the ForgeSolar analysis.



Figure 9. Residential and Non-Residential Buildings within 1 Mile Radius (Yellow Circle) of the Center of the Proposed Solar Facility Modeled in ForgeSolar (Observation Points, OP)

The SGHAT results for the Project were **no glare** of any intensity during any minute of the year for any of the observation points located at buildings. The four additional ForgeSolar models representing intelligent backtracking of the array near sunrise and sunset predicted **no glare** from a backtracking array for any of the observation points located at buildings.

SGHAT Results

As described above, the ForgeSolar SGHAT software was used to conduct a glare hazard analysis of pilots landing at Travis Air Force Base, air traffic controllers at Travis Air Force Base, motorists on Lake Herman Road, and people at nearby buildings. A summary of results is presented in this section of the report and the full ForgeSolar-generated report in provided in Appendix A.

The ForgeSolar SGHAT defines two intensities of glare, "green" and "yellow". Green glare represents a "Low Potential for Temporary After-Image" and is about 1/1000th the intensity of looking directly into

the sun (based on Hazards Plot in the SGHAT User's Manual)⁴. According to the FAA Interim solar policy⁵, which defines the requirements for solar projects constructed on airport property, glare visible to pilots on their final landing approach that is classified in this green range is acceptable. In other words, any amount of green glare is considered non-hazardous. Yellow glare has a "Potential for Temporary After-Image"; such glare could affect the pilot's ability so see clearly even after looking away from the glare. The FAA Interim solar policy (which only has authority for solar built on airports) does not allow solar arrays that produce yellow glare visible to pilots on final approach to be built on airport property. The ForgeSolar results use the same green and yellow glare classifications for glare visible at other types of observation points as well, such as to motorists and pedestrians.

The ForgeSolar SGHAT results for the Project were **no glare** of any intensity during any minute of the year for every flight path, air traffic control tower, roadway route, and the land-based observation point. As described in the *Modeling the Lake Herman Solar Facility* section, additional ForgeSolar models were constructed to simulate intelligent backtracking by the tracking system early and late in the day to avoid inter-row shading. When backtracking the modules are turned away from the sun and thus have more potential to create a glare hazard. The results of these simulations showed that backtracked rows (45 and 30 degrees from horizontal) did not produce any glare during the hours near sunrise and sunset in which backtracking may be used. The models did predict some glare near noon, but this glare result is meaningless because the array will be tracking the sun at this time of day and not in a backtracked position at that time. The ForgeSolar-generated reports for the 30-tilt east-facing and west-facing are provided in Appendix C respectively.

Conclusion

The solar glare hazard analysis of the proposed Lake Herman solar facility finds that the PV system will not produce any glare hazards. ForgeSolar, a detailed, proven solar glare hazard analysis software, was used to model the potential for the proposed solar array to cause glare for approaching motorists, people at nearby buildings, and pilots and air traffic controllers at Travis Air Force Base. In fact, the software analysis found **no glare of any intensity at any time during the year at any of the analyzed locations**. The proposed PV project uses a single-axis tracking racking system to support the solar modules/panels which keeps the solar modules generally facing toward the sun. This design avoids situations where the sunlight hits the solar panels with a glancing angle, which is when the glass of a solar panel is reflective and thus has a potential to cause visible glare to an observer.

⁴ Solar Glare Hazard Analysis Tool Users Manual version 2.0,

 $https://share.sandia.gov/phlux/static/references/glint-glare/SGHAT_Users_Manual_v2-0_final.pdf$

⁵ Interim Policy for the FAA Review of Solar Energy System Projects on Federally Obligated Airports,

http://www.gpo.gov/fdsys/pkg/FR-2013-10-23/pdf/2013-24729.pdf

Appendix A: SGHAT/ForgeSolar Results Report

ForgeSolar Glare Analysis Report – Page 1 of 13



SITE CONFIGURATION

Analysis Parameters

DNI: peaks at 1,000.0 W/m^2 Time interval: 1 min Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad Site Config ID: 29667.5349



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PV Array(s)

Name: PV array Axis tracking: Single-axis rotation Tracking axis orientation: 180.0° Tracking axis tilt: 0.0° Tracking axis panel offset: 0.0° Max tracking angle: 60.0° Resting angle: 60.0° Rated power: 5000.0 kW Panel material: Smooth glass without AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	38.096105	-122.144826	106.95	5.00	111.95
2	38.096333	-122.144794	108.88	5.00	113.88
3	38.098021	-122.143334	116.12	5.00	121.12
4	38.098013	-122.142798	130.51	5.00	135.51
5	38.097633	-122.142798	145.05	5.00	150.05
6	38.097641	-122.142637	150.85	5.00	155.85
7	38.098004	-122.142390	142.65	5.00	147.65
8	38.097996	-122.142004	150.95	5.00	155.95
9	38.098781	-122.142026	154.44	5.00	159.44
10	38.098781	-122.141607	158.77	5.00	163.77
11	38.099288	-122.141629	142.58	5.00	147.58
12	38.099566	-122.141350	161.93	5.00	166.93
13	38.099566	-122.140309	188.83	5.00	193.83
14	38.099229	-122.140169	193.00	5.00	198.00
15	38.098798	-122.140212	183.89	5.00	188.89
16	38.098798	-122.139955	182.04	5.00	187.04
17	38.098232	-122.139923	168.46	5.00	173.46
18	38.097692	-122.140008	160.23	5.00	165.23
19	38.097244	-122.139987	146.89	5.00	151.89
20	38.097211	-122.139730	139.04	5.00	144.04
21	38.096620	-122.139751	131.05	5.00	136.05
22	38.096240	-122.139944	121.39	5.00	126.39
23	38.095843	-122.139955	115.49	5.00	120.50
24	38.095547	-122.141017	145.56	5.00	150.56
25	38.095573	-122.144407	128.45	5.00	133.45
26	38.095826	-122.144847	104.06	5.00	109.06

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Name: F	Bunway	031				
Descrip	nunway	USL		and the second second		111
Thresho	old heig	ht: 75 ft				
Directio	on: 47.0°	,		1		A CONTRACTOR
Glide SI Pilot vie	lope: 3.0 ew restri	icted? Yes				11/2 /1
Vertical	l view: 3	0.0°				14
Azimuth	hal view	r: 50.0°		Google	PriveZ019. DistalGlobe, U.S. Geological Sur	vey. USDA Farm Service Agency
Point	ıt	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Three	shold	38.243510	-121.956684	32.62	75.00	107.63
Two-	mile	38.223792	-121.983639	3.64	657.44	661.08
Directio Glide sl Pilot vie Vertical Azimuth	old heig on: 47.0° lope: 3.0 ew restri I view: 3 hal view	ht: 69 ft)° icted? Yes 0.0° :: 50.0°			R	
Directio Glide sl Pilot vie Vertical Azimuth	old heig on: 47.0° lope: 3.0 ew restri I view: 3 hal view	ht: 69 ft icted? Yes 0.0° :: 50.0°		Google	ery 22019, DigitalGable, U.S. Geological Sur	Veg. USDA Farm Service Agency
Directio Glide sl Pilot vie Vertical Azimuth	old heig on: 47.0° lope: 3.0 ew restri I view: 3 hal view	ht: 69 ft icted? Yes 0.0° 1: 50.0° Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	ver, USDA Farm Serve Agency Total elevation (ft)
Directio Glide sl Pilot vie Vertical Azimuth Point Three Two-	old heig on: 47.0° lope: 3.0 ew restri I view: 30 hal view that view	ht: 69 ft ; icted? Yes 0.0° : 50.0° Latitude (°) 38.261684 38.241965	Longitude (°) -121.926204 -121.953166	Google Ground elevation (ft) 52.29 19.57	ry 2019, Dytafökke, U.S. Geological Sur Height above ground (ft) 699.00 655.17	Vey, USDA Farm Service Agents Total elevation (ft) 121.29 674.75
Directio Glide sl Pilot vie Vertical Azimuth Thresh Directio Glide sl Pilot vie Vertical Azimuth	old heig on: 47.0° lope: 3.0 ew restril I view: 3.1 hal view hal view hal view hal view shold mile Runway : otion: old heig on: 226.9 lope: 3.0 ew restri I view: 3.1 hal view	ht: 69 ft jo icted? Yes 0.0° 2: 50.0° Latitude (°) 38.261684 38.241965 212 (assault strip ht: 50 ft jo icted? Yes 0.0° : 50.0°	Longitude (°) -121.926204 -121.953166	Ground elevation (tt) 52.29 19.57	42019, Departement 0.5 Geodesice 0.5 Geodesice 0.6	Very USA Ferr Served Agency Total elevation (ft) 121.29 674.75
Directio Glide si Pilot viev Vertical Azimuth Point Three Two- Directio Glide si Pilot viev Vertical Azimuth	old heig on: 47.0° lope: 3.0 ew restri I view: 30 hal view shold mile Runway: old heig on: 226.9 lope: 3.0 ew restri I view: 3 hal view	ht: 69 ft j° icted? Yes 0.0° : 50.0° Latitude (°) 38.261684 38.241965 212 (assault strip ht: 50 ft j° icted? Yes 0.0° : 50.0° Latitude (°)	Longitude (°) -121.926204 -121.953166	Ground elevation (ft) 52.29 19.57	Height above ground (ft)	Very, UEDA Farm Served Agency Total elevation (ft) 121.29 674.75
Point Point Point Point Point Point Point Point	old heig on: 47.0° lope: 3.0 ew restri I view: 3/ hal view hal view nt shold mile Runway: old heig on: 226.9 lope: 3.0 ew restri I view: 3/ hal view	ht: 69 ft icted? Yes 0.0° : 50.0° Latitude (°) 38.261684 38.241965 212 (assault strip ht: 50 ft j° icted? Yes 0.0° : 50.0°	 Longitude (°) -121.926204 -121.953166 >> >><!--</td--><td>Ground elevation (ft) 52.29 19.57</td><td>Height above ground (ft) 655.17 Field of the second of t</td><td>Vey, USDA Farm Serve Adercy Total elevation (ft) 121.29 674.75 Vey, USDA Farm Serve Adercy Vey, USDA Farm Serve Adercy Total elevation (ft)</td>	Ground elevation (ft) 52.29 19.57	Height above ground (ft) 655.17 Field of the second of t	Vey, USDA Farm Serve Adercy Total elevation (ft) 121.29 674.75 Vey, USDA Farm Serve Adercy Vey, USDA Farm Serve Adercy Total elevation (ft)

ForgeSolar Glare Analysis Report – Page 5 of 13

Description: Threshold heig Direction: 227. Glide slope: 3. Pilot view restr Vertical view: S Azimuthal view	21L jht: 75 ft 0° 0° iricted? Yes 80.0° v: 50.0°		Google		vej. USDA Perm Service Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold	38.281560	-121.898514	53.07	75.00	128.08
Two-mile	38.301279	-121.871545	37.42	644.11	681.53
Vertical view: 3	r icted? Yes 30.0°		6	40	104
Vertical view: (Azimuthal view	ricted? Yes 80.0° v: 50.0°	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	ver, USDA Farm Service Agency Total elevation (ff)
Point	ricted? Yes 80.0° v: 50.0° Latitude (°) 28.263417	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	ver, USDA Familianov Agency Total elevation (ft)
Vertical view result Azimuthal view Point Threshold Two-mile	ricted? Yes 30.0° r: 50.0° Latitude (°) 38.263417 38.283136	Longitude (°) -121.928980 -121.902017	Google Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18	vey, USDA Ferm Service Agency Total elevation (ft) 123.70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3.1, Vertical view restu Vertical view: 3 Azimuthal view	ricted? Yes 30.0° r: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip) 31.50 ft 0° ricted? Yes 30.0° r: 50.0°	Longitude (°) -121.928980 -121.902017	Coogle Ground elevation (ft) 48.70 46.98	ey 2015 . Dybriddoo U.S. Georgiel Gre Height above ground (ft) 75.00 630.18	vey, USDA Familiario Agency Total elevation (ft) 123.70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3.1 Pilot view rest Vertical view: 3 Azimuthal view Point Point	icted? Yes 30.0° icted? Yes 38.263417 38.263417 38.283136 32 (assault strip) 31 50 ft 0° icted? Yes 30.0° icted? Yes 30.0° Latitude (")	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18	Very, USDA Farm Service Agency Total elevation (ft) 123.70 677.15
Point Threshold new rest Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3.1 Pilot view rest Vertical view: 3 Azimuthal view Point Threshold	icted? Yes 30.0° Latitude (°) 38.263417 38.283136 32 (assault strip) 31.50 ft 0° ricted? Yes 30.0° Latitude (°) 38.273315	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98 Ground elevation (ft) Ground elevation (ft) 58.49	Height above ground (H) 75.00 630.18	ver, USDA Farm Service Agency Total elevation (ft) 123.70 677.15

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Discrete Observation Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
OP 1	1	38.099556	-122.143422	116.45	6.00
OP 2	2	38.105524	-122.148023	186.99	6.00
OP 3	3	38.101159	-122.130236	392.05	6.00
OP 4	4	38.090553	-122.132693	254.76	6.00
OP 5	5	38.089899	-122.147898	204.10	6.00
OP 6	6	38.089743	-122.147560	202.99	6.00
OP 7	7	38.089662	-122.147346	201.52	6.00
OP 8	8	38.089502	-122.147077	198.72	6.00
OP 9	9	38.089316	-122.146900	198.50	6.00
OP 10	10	38.089109	-122.146788	196.28	6.00
OP 11	11	38.088932	-122.146535	191.32	6.00
OP 12	12	38.088835	-122.146262	189.79	6.00
OP 13	13	38.088733	-122.146037	187.96	6.00
OP 14	14	38.088641	-122.145629	188.97	6.00
OP 15	15	38.088691	-122.145345	190.06	6.00
OP 16	16	38.088522	-122.145076	189.01	6.00
OP 17	17	38.088964	-122.149402	220.54	6.00
OP 18	18	38.088617	-122.151312	249.51	6.00
OP 19	19	38.087342	-122.155356	248.27	6.00
20-ATCT	20	38.265538	-121.933272	51.83	100.00
OP 21	21	38.089387	-122.140280	42.90	6.00
OP 22	22	38.086251	-122.139004	41.33	6.00

Map image of 20-ATCT



Route Receptor(s)

Name: Route 1 Path type: Two-way Observer view angle: 50.0°



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	38.098603	-122.156958	147.86	3.50	151.36
2	38.098464	-122.154163	151.17	3.50	154.67
3	38.098411	-122.152891	146.38	3.50	149.88
4	38.098283	-122.152460	145.63	3.50	149.13
5	38.097681	-122.151210	127.57	3.50	131.07
6	38.097535	-122.150708	114.88	3.50	118.38
7	38.097267	-122.148975	103.07	3.50	106.57
8	38.097105	-122.148418	117.17	3.50	120.67
9	38.096507	-122.146875	85.81	3.50	89.31
10	38.095543	-122.145159	100.36	3.50	103.86
11	38.095207	-122.144547	120.38	3.50	123.88
12	38.095026	-122.144196	127.21	3.50	130.71
13	38.094924	-122.143858	131.01	3.50	134.51
14	38.094922	-122.143316	134.99	3.50	138.49
15	38.095232	-122.140725	137.78	3.50	141.28
16	38.095517	-122.138239	136.33	3.50	139.83
17	38.095431	-122.137447	148.37	3.50	151.87
18	38.095277	-122.137005	148.82	3.50	152.32
19	38.095045	-122.136624	145.33	3.50	148.83
20	38.094711	-122.136243	139.69	3.50	143.19
21	38.093616	-122.134698	130.76	3.50	134.26
22	38.092566	-122.132939	153.79	3.50	157.29
23	38.091918	-122.131833	176.45	3.50	179.95
24	38.091621	-122.130903	182.10	3.50	185.60
25	38.091015	-122.128041	180.03	3.50	183.53
26	38.090618	-122.125619	197.60	3.50	201.10

GLARE ANALYSIS RESULTS

Summary of Glare

PV Array Name	Tilt	Orient	"Green" Glare	"Yellow" Glare	Energy
	(°)	(°)	min	min	kWh
PV array	SA	SA	0	0	15,490,000.0
	tracking	tracking			

Total annual glare received by each receptor

Receptor	Annual Green Glare (min)	Annual Yellow Glare (min)		
Runway 03L	0	0		
Runway 03R	0	0		
Runway 212 (assault strip)	0	0		
Runway 21L	0	0		
Runway 21R	0	0		
Runway 32 (assault strip)	0	0		
OP 1	0	0		
OP 2	0	0		
OP 3	0	0		
OP 4	0	0		
OP 5	0	0		
OP 6	0	0		
OP 7	0	0		
OP 8	0	0		
OP 9	0	0		
OP 10	0	0		
OP 11	0	0		
OP 12	0	0		
OP 13	0	0		
OP 14	0	0		
OP 15	0	0		
OP 16	0	0		
OP 17	0	0		
OP 18	0	0		
OP 19	0	0		
20-ATCT	0	0		
OP 21	0	0		
Receptor	Annual Green Glare (min)	Annual Yellow Glare (min)		
----------	--------------------------	---------------------------		
OP 22	0	0		
Route 1	0	0		

Results for: PV array

Receptor	Green Glare (min)	Yellow Glare (min)
Runway 03L	0	0
Runway 03R	0	0
Runway 212 (assault strip)	0	0
Runway 21L	0	0
Runway 21R	0	0
Runway 32 (assault strip)	0	0
OP 1	0	0
OP 2	0	0
OP 3	0	0
OP 4	0	0
OP 5	0	0
OP 6	0	0
OP 7	0	0
OP 8	0	0
OP 9	0	0
OP 10	0	0
OP 11	0	0
OP 12	0	0
OP 13	0	0
OP 14	0	0
OP 15	0	0
OP 16	0	0
OP 17	0	0
OP 18	0	0
OP 19	0	0
20-ATCT	0	0
OP 21	0	0
OP 22	0	0
Route 1	0	0

Flight Path: Runway 03L

0 minutes of yellow glare 0 minutes of green glare

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Flight Path: Runway 03R

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 212 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21L

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21R

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 32 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 1

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 2

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 3

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 4

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 5

0 minutes of yellow glare

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0 minutes of green glare

Point Receptor: OP 6

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 7

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 8

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 9

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 10

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 11

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 12

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 13

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 14

0 minutes of yellow glare 0 minutes of green glare

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Point Receptor: OP 15

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 16

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 17

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 18

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 19

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: 20-ATCT

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 21

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 22

0 minutes of yellow glare 0 minutes of green glare

Route: Route 1

0 minutes of yellow glare 0 minutes of green glare

Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and

geographic obstructions.

Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections

will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.

The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual results and glare occurrence may differ.

Hazard zone boundaries shown in the Giare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

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Appendix B: SGHAT/ForgeSolar Results Report for Sunrise Backtrack Simulation

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 1 of 13



ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 2 of 13

SITE CONFIGURATION

Analysis Parameters

DNI: peaks at 1,000.0 W/m^2 Time interval: 1 min Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad Site Config ID: 29690.5349



ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 3 of 13

PV Array(s)

Name: PV array Axis tracking: Fixed (no rotation) Tilt: 30.0° Orientation: 90.0° Rated power: 5000.0 kW Panel material: Smooth glass without AR coating Reflectivity: Vary with sun Slope error: correlate with material



1	38.096105	-122 144826			
2		-122.144020	106.95	5.00	111.95
	38.096333	-122.144794	108.88	5.00	113.88
3	38.098021	-122.143334	116.12	5.00	121.12
4	38.098013	-122.142798	130.51	5.00	135.51
5	38.097633	-122.142798	145.05	5.00	150.05
6	38.097641	-122.142637	150.85	5.00	155.85
7	38.098004	-122.142390	142.65	5.00	147.65
8	38.097996	-122.142004	150.95	5.00	155.95
э	38.098781	-122.142026	154.44	5.00	159.44
10	38.098781	-122.141607	158.77	5.00	163.77
11	38.099288	-122.141629	142.58	5.00	147.58
12	38.099566	-122.141350	161.93	5.00	166.93
13	38.099566	-122.140309	188.83	5.00	193.83
14	38.099229	-122.140169	193.00	5.00	198.00
15	38.098798	-122.140212	183.89	5.00	188.89
16	38.098798	-122.139955	182.04	5.00	187.04
17	38.098232	-122.139923	168.46	5.00	173.46
18	38.097692	-122.140008	160.23	5.00	165.23
19	38.097244	-122.139987	146.89	5.00	151.89
20	38.097211	-122.139730	139.04	5.00	144.04
21	38.096620	-122.139751	131.05	5.00	136.05
22	38.096240	-122.139944	121.39	5.00	126.39
23	38.095843	-122.139955	115.49	5.00	120.50
24	38.095547	-122.141017	145.56	5.00	150.56
25	38.095573	-122.144407	128.45	5.00	133.45
26	38.095826	-122.144847	104.06	5.00	109.06

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 4 of 13

Name: Runway Description: Threshold hei Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view	r 03L ght: 75 ft ₀° °ricted? Yes 30.0° w: 50.0°				
			Google	pery 62019 , DigitalGlobe, U.S. Geological Sur	vey, USDA Farm Service Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold Two-mile	38.243510 38.223792	-121.956684	32.62	75.00	107.63
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view	gnt: 69 ft 0° ricted? Yes 30.0° w: 50.0°			R	
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: Azimuthal view	gnt: 69 ft j° 0° ricted? Yes 30.0° w: 50.0° Latitude (°)	Longitude (°)	Google Ground elevation (ft)	er soorte de la constante de l	Very LUCA Ferm Served Agency Total elevation (ft)
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: 4 Azimuthal view Point Threshold	gnt: 69 ft 0° ricted? Yes 30.0° w: 50.0° Latitude (°) 38.261684	Longitude (°) -121.926204	Google Ground elevation (ft) 52.29	ry 2019, Dytafdide, U.S. Geological Sur Height above ground (ft) 59.00	vey, USDA Farm Servee Agency Total elevation (ft) 121.29
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: Azimuthal view Point Threshold Two-mile	int: 69 ft 0° ricted? Yes 30.0° w: 50.0° Latitude (°) 38.261684 38.241965	Longitude (°) -121.926204 -121.953166	Google Ground elevation (ft) 52.29 19.57	42019, Downlabor, U.S. Gewongen Kar Height above ground (ft) 89.00 655.17	Ver, LUCA Form Server Agency Total elevation (ft) 121.28 674.75
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: 4 Azimuthal view Point Threshold Two-mile Name: Runway Description: Threshold heij Direction: 226 Glide slope: 3. Pilot view rest Vertical view: 4 Azimuthal view	gnt: 69 ft ^{jo} 0° ricted? Yes 30.0° v : 50.0° Latitude (°) 38.261684 38.241965 v 212 (assault strij ght: 50 ft 9° 0° ricted? Yes 30.0° w: 50.0°	Longitude (°) -121.926204 -121.953166	Ground elevation (ft) 52.29 19.57	Height above ground (ft) 655.17 655.17	vey, USDA Farm Service Agency Total elevation (ft) 121.29 674.75
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: : Azimuthal view Point Threshold Two-mile Name: Runway Description: Threshold heip Direction: 226 Glide slope: 3 Pilot view rest Vertical view: : Azimuthal view	Int: 69 ft o° ricted? Yes 30.0° w: 50.0° Latitude (°) 38.261684 38.241965 v 212 (assault stri ght: 50 ft .9° o° ricted? Yes 30.0° w: 50.0° Latitude (°)	Longitude (°) -121.926204 -121.953166 p)	Ground elevation (ft) 52.29 19.57	Height above ground (ft) (50) - 2019 - Dysafekker, U.S. Geological Sur Height above ground (ft) (55) - 17 (50) - 10 (50) - 10	vey, USDA Farm Servee Agency Total elevation (ft) 121.29 674.75

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 5 of 13

Description: Threshold heig Direction: 227. Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view	21L ght: 75 ft 0° 0° ricted? Yes 30.0° v: 50.0°		Google	eg 62019. Ogsatölser, U.S. Geosgeal Sar	vej, USDA Parm Servee Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold	38.281560	-121.898514	53.07	75.00	128.08
Two-mile	38.301279	-121.871545	37.42	644.11	681.53
transiant sile	0.09				and the second se
vertical view: 3	30.0° v : 50.0°		Google	ery £2019, Dytal/Sible, U.S. Geological Sur	vey, USDA Farm Service Agency
vertical view: 3 Azimuthal view Point	30.0° v: 50.0° Latitude (°)	Longitude (°)	Google Ground elevation (ft)	Height above ground (ft)	ver, USDA Furm Service Agency Total elevation (ft)
Azimuthal view Azimuthal view Point Threshold Two-mile	80.0° v: 50.0° Latitude (°) 38.263417 38.283136	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18	vey, USDA Familiservoe Agency Total elevation (ft) 123.70 677.15
Vertical view: 3 Azimuthal view Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3: Pilot view rest Vertical view: 3	80.0° v: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip) ght: 50 ft 0° ricted? Yes 30.0° v: 50.0°	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18	ver, USDA Parm Service Agency Total elevation (ft) 123.70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3: Pilot view rest Vertical view: 3 Azimuthal view Point Point	80.0° v: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip ght: 50 ft 0° ricted? Yes 30.0° v: 50.0°	Longitude (°)	Ground elevation (ft) 48.70 46.98	Height above ground (ff) 630.18	ver, USDA Firm Service Agency Total elevation (ft) 123.70 677.15
Point Threshold new: 3 Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Gilde slope: 3: Pilot view rest Vertical view: 3 Azimuthal view Point Threshold	80.0° w: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip ght: 50 ft o° ricted? Yes 30.0° w: 50.0° Latitude (°) 38.273315	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98	Height above ground (H) 630.18	ver, USDA Firm Service Agency Total elevation (ft) 123.70 677.15

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 6 of 13

Discrete Observation Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
OP 1	1	38.099556	-122.143422	116.45	6.00
OP 2	2	38.105524	-122.148023	186.99	6.00
OP 3	з	38.101159	-122.130236	392.05	6.00
OP 4	4	38.090553	-122.132693	254.76	6.00
OP 5	5	38.089899	-122.147898	204.10	6.00
OP 6	6	38.089743	-122.147560	202.99	6.00
OP 7	7	38.089662	-122.147346	201.52	6.00
OP 8	8	38.089502	-122.147077	198.72	6.00
OP 9	9	38.089316	-122.146900	198.50	6.00
OP 10	10	38.089109	-122.146788	196.28	6.00
OP 11	11	38.088932	-122.146535	191.32	6.00
OP 12	12	38.088835	-122.146262	189.79	6.00
OP 13	13	38.088733	-122.146037	187.96	6.00
OP 14	14	38.088641	-122.145629	188.97	6.00
OP 15	15	38.088691	-122.145345	190.06	6.00
OP 16	16	38.088522	-122.145076	189.01	6.00
OP 17	17	38.088964	-122.149402	220.54	6.00
OP 18	18	38.088617	-122.151312	249.51	6.00
OP 19	19	38.087342	-122.155356	248.27	6.00
20-ATCT	20	38.265538	-121.933272	51.83	100.00

Map image of 20-ATCT



ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page7 of 13

Route Receptor(s)

Name: Route 1 Path type: Two-way Observer view angle: 50.0°



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	38.098603	-122.156958	147.86	3.50	151.36
2	38.098464	-122.154163	151.17	3.50	154.67
3	38.098411	-122.152891	146.38	3.50	149.88
4	38.098283	-122.152460	145.63	3.50	149.13
5	38.097681	-122.151210	127.57	3.50	131.07
6	38.097535	-122.150708	114.88	3.50	118.38
7	38.097267	-122.148975	103.07	3.50	106.57
8	38.097105	-122.148418	117.17	3.50	120.67
9	38.096507	-122.146875	85.81	3.50	89.31
10	38.095543	-122.145159	100.36	3.50	103.86
11	38.095207	-122.144547	120.38	3.50	123.88
12	38.095026	-122.144196	127.21	3.50	130.71
13	38.094924	-122.143858	131.01	3.50	134.51
14	38.094922	-122.143316	134.99	3.50	138.49
15	38.095232	-122.140725	137.78	3.50	141.28
16	38.095517	-122.138239	136.33	3.50	139.83
17	38.095431	-122.137447	148.37	3.50	151.87
18	38.095277	-122.137005	148.82	3.50	152.32
19	38.095045	-122.136624	145.33	3.50	148.83
20	38.094711	-122.136243	139.69	3.50	143.19
21	38.093616	-122.134698	130.76	3.50	134.26
22	38.092566	-122.132939	153.79	3.50	157.29
23	38.091918	-122.131833	176.45	3.50	179.95
24	38.091621	-122.130903	182.10	3.50	185.60
25	38.091015	-122.128041	180.03	3.50	183.53
26	38.090618	-122.125619	197.60	3.50	201.10

GLARE ANALYSIS RESULTS

Summary of Glare

PV Array Name	Tilt	Orient	"Green" Glare	"Yellow" Glare	Energy
	(°)	(°)	min	min	kWh
PV array	30.0	90.0	3,743	0	9,191,000.0

Total annual glare received by each receptor

Receptor	Annual Green Glare (min)	Annual Yellow Glare (min)
Runway 03L	0	0
Runway 03R	0	0
Runway 212 (assault strip)	0	0
Runway 21L	0	0
Runway 21R	0	0
Runway 32 (assault strip)	0	0
OP 1	0	0
OP 2	0	0
OP 3	3697	0
OP 4	0	0
OP 5	0	0
OP 6	0	0
OP 7	0	0
OP 8	0	0
OP 9	0	0
OP 10	0	0
OP 11	0	0
OP 12	0	0
OP 13	0	0
OP 14	0	0
OP 15	0	0
OP 16	0	0
OP 17	0	0
OP 18	0	0
OP 19	0	0
20-ATCT	46	0
Route 1	0	0

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 9 of 13

Receptor	Green Glare (min)	Yellow Glare (min)
Runway 03L	0	0
Runway 03R	0	0
Runway 212 (assault strip)	0	0
Runway 21L	0	0
Runway 21R	0	0
Runway 32 (assault strip)	0	0
OP 1	0	0
OP 2	0	0
OP 3	3697	0
OP 4	0	0
OP 5	0	0
OP 6	0	0
OP 7	0	0
OP 8	0	0
OP 9	0	0
OP 10	0	0
OP 11	0	0
OP 12	0	0
OP 13	0	0
OP 14	0	0
OP 15	0	0
OP 16	0	0
OP 17	0	0
OP 18	0	0
OP 19	0	0
20-ATCT	46	0
Route 1	0	0

Results for: PV array

Flight Path: Runway 03L

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 03R

0 minutes of yellow glare 0 minutes of green glare

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) - Page 10 of 13

Flight Path: Runway 212 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21L

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21R

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 32 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 1

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 2

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 3

0 minutes of yellow glare 3697 minutes of green glare





ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) – Page 11 of 13

Point Receptor: OP 4

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 5

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 6

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 7

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 8

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 9

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 10

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 11

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 12

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 13

0 minutes of yellow glare

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) - Page 12 of 13

0 minutes of green glare

Point Receptor: OP 14

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 15

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 16

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 17

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 18

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 19

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: 20-ATCT

0 minutes of yellow glare 46 minutes of green glare

ForgeSolar Glare Analysis Report (Sunrise Backtrack Simulation) - Page 13 of 13



Route: Route 1

0 minutes of vellow glare 0 minutes of green glare

Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.

Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.

The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.

The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual results and glare occurrence may differ

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

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Appendix C: SGHAT/ForgeSolar Results Report for Sunset Backtrack Simulation

ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) - Page 1 of 13



Site configuration: west facing 30 fixed tilt to simulate backtracking Analysis conducted by Tommy Cleveland (thcleveland@gmail.com) at 02:28 on 21 Jul, 2019.

U.S. FAA 2013 Policy Adherence

The following table summarizes the policy adherence of the glare analysis based on the 2013 U.S. Federal Aviation Administration Interim Policy 78 FR 63276. This policy requires the following criteria be met for solar energy systems on airport property:

- · No "yellow" glare (potential for after-image) for any flight path from threshold to 2 miles
- · No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- · Default analysis and observer characteristics (see list below)

ForgeSolar does not represent or speak officially for the FAA and cannot approve or deny projects. Results are informational only.

COMPONENT	STATUS	DESCRIPTION
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable
Flight path(s)	PASS	Flight path receptor(s) do not receive yellow glare
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare

Default glare analysis parameters and observer eye characteristics (for reference only):

- · Analysis time interval: 1 minute
- · Ocular transmission coefficient: 0.5
- · Pupil diameter: 0.002 meters
- · Eye focal length: 0.017 meters

Project: Lake Herman

· Sun subtended angle: 9.3 milliradians

FAA Policy 78 FR 63276 can be read at https://www.federalregister.gov/d/2013-24729

ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 2 of 13

SITE CONFIGURATION

Analysis Parameters

DNI: peaks at 1,000.0 W/m*2 Time interval: 1 min Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad Site Contig ID: 29688.5349



ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 3 of 13

PV Array(s)

Name: PV array Axis tracking: Fixed (no rotation) Tilt: 30.0° Orientation: 270.0° Rated power: 5000.0 kW Panel material: Smooth glass without AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	38.096105	-122.144826	106.95	5.00	111.95
2	38.096333	-122.144794	108.88	5.00	113.88
3	38.098021	-122.143334	116.12	5.00	121.12
4	38.098013	-122.142798	130.51	5.00	135.51
5	38.097633	-122.142798	145.05	5.00	150.05
6	38.097641	-122.142637	150.85	5.00	155.85
7	38.098004	-122.142390	142.65	5.00	147.65
8	38.097996	-122.142004	150.95	5.00	155.95
9	38.098781	-122.142026	154.44	5.00	159.44
10	38.098781	-122.141607	158.77	5.00	163.77
11	38.099288	-122.141629	142.58	5.00	147.58
12	38.099566	-122.141350	161.93	5.00	166.93
13	38.099566	-122.140309	188.83	5.00	193.83
14	38.099229	-122.140169	193.00	5.00	198.00
15	38.098798	-122.140212	183.89	5.00	188.89
16	38.098798	-122.139955	182.04	5.00	187.04
17	38.098232	-122.139923	168.46	5.00	173.46
18	38.097692	-122.140008	160.23	5.00	165.23
19	38.097244	-122.139987	146.89	5.00	151.89
20	38.097211	-122.139730	139.04	5.00	144.04
21	38.096620	-122.139751	131.05	5.00	136.05
22	38.096240	-122.139944	121.39	5.00	126.39
23	38.095843	-122.139955	115.49	5.00	120.50
24	38.095547	-122.141017	145.56	5.00	150.56
25	38.095573	-122.144407	128.45	5.00	133.45
26	38.095826	-122.144847	104.06	5.00	109.06

ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 4 of 13

Name: Runway Description: Threshold heig	7 03L ght: 75 ft		T	$\boldsymbol{\checkmark}$	
Direction: 47.0 Glide slope: 3.	ەر .0°		2		CS LAND
Pilot view rest	ricted? Yes		1		14
vertical view:	30.0° ₩: 50.0°		Google	pry 62019, Digta/Globe, U.S. Geological Sur	vey, USDA Farm Service Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold	38.243510	-121.956684	32.62	75.00	107.63
Two-mile	38.223792	-121.983639	3.64	657.44	661.08
Direction: 47.0 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view	ı° 0° ; ricted? Yes 30.0° w : 50.0°		Google	Pry 22019, DigitalGlobe, U.S. Geological Sur	ver, USDA Farm Service Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold	38.261684	-121.926204	52.29	69.00	121.29
Name: Runway Description: Threshold hei Direction: 226 Glide slope: 3 Pilot view rest Vertical view: Azimuthal view	⁷ 212 (assault stri ght: 50 ft .0° . ricted? Yes 30.0° w: 50.0°	۵)		1	
	l atitude (°)	Longitude (°)	Google Ground elevation (ft)	rery 62019 , DigitalGlobe, U.S. Geological Sur Height above ground (ft)	vey, USDA Farm Service Agency Total elevation (ft)
Point		-			
Point Threshold	38.280787	-121.897193	52.14	50.00	102.14

ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 5 of 13

Description: Threshold heig Direction: 227. Glide slope: 3. Pilot view rest Vertical view: { Azimuthal viev	21L jht: 75 ft 0° 1° 1° icted? Yes 80.0° 1°: 50.0°		Google	ey 2019. OptaGize, U.S. Geospathar	vej. USDA Farm Service Agency
Point	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
Threshold	38.281560	-121.898514	53.07	75.00	128.08
Two-mile	38.301279	-121.871545	37.42	644.11	681.53
vertical view: a	30.0° r : 50.0°		Google	ery (2019, DigtalGable, U.S. Geological Sur	vey, USDA Farm Service Agency
Point	80.0° v: 50.0° Latitude (°)	Longitude (°)	Google Ground elevation (ft)	ery EX112 DiptalGlobe, U.S. Geological Sur Height above ground (ff)	ver, USDA Ferm Service Agency Total elevation (ft)
Point	80.0° v: 50.0° Latitude (°) 38.263417	Longitude (°) -121.928980	Ground elevation (ft) 48.70	Height above ground (ft) 75.00	ver, USDA Furm Service Agency Total elevation (ft) 123.70 077.1 fr
Point Threshold Two-mile Name: Runway	00.0° v: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip)	Longitude (°) -121.928980 -121.902017	Google Ground elevation (ft) 48.70 46.98	Height above ground (ff) 75.00 630.18	ver, USDA Ferm Service Agency Total elevation (ft) 123 70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3: Pilot view rest Vertical view: 2 Azimuthal view	00.0° x: 50.0° Latitude (°) 38.263417 38.263417 38.283136 32 (assault strip) jht: 50 ft op ficted? Yes 80.0°	Longitude (°) -121.928980 -121.902017	Coogle Ground elevation (ft) 48.70 46.98	Height above ground (ff) 75.00 630.18	ver, USDA Firm Service Agency Total elevation (ft) 123 70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view	00.0° x: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip) pht: 50 ft po ricted? Yes 80.0° x: 50.0°	Longitude (°) -121.928980 -121.902017	Coogle Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18	Vey, USDA Firm Service Agency Total elevation (ft) 123 70 677.15
Point Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view Point	00.0° x: 50.0° Latitude (°) 38.263417 38.263417 38.283136 32 (assault strip) ght: 50 ft 0° ricted? Yes 30.0° x: 50.0° Latitude (°)	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98	Height above ground (ft) 75.00 630.18 Filler Filler Height above ground (ft)	vey, USDA Fam Service Agency Total elevation (ft) 123.70 677.15 Vey, USDA Fam Service Agency vey, USDA Fam Service Agency Total elevation (ft)
Point Threshold Two-mile Name: Runway Description: Threshold heig Direction: 46.4 Glide slope: 3. Pilot view rest Vertical view: 3 Azimuthal view Point Threshold	00.0° x: 50.0° Latitude (°) 38.263417 38.283136 32 (assault strip) ght: 50 ft 0° ricted? Yes 30.0° x: 50.0° Latitude (°) 38.273915	Longitude (°) -121.928980 -121.902017	Ground elevation (ft) 48.70 46.98 46	Height above ground (ft) 75.00 630.18	ver, USDA Fam Service Agency Total elevation (ft) 123.70 677.15

ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 6 of 13

Discrete Observation Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
OP 1	1	38.099556	-122.143422	116.45	6.00
OP 2	2	38.105524	-122.148023	186.99	6.00
OP 3	Э	38.101159	-122.130236	392.05	6.00
OP 4	4	38.090553	-122.132693	254.76	6.00
OP 5	5	38.089899	-122.147898	204.10	6.00
OP 6	6	38.089743	-122.147560	202.99	6.00
OP 7	7	38.089662	-122.147346	201.52	6.00
OP 8	8	38.089502	-122.147077	198.72	6.00
OP 9	9	38.089316	-122.146900	198.50	6.00
OP 10	10	38.089109	-122.146788	196.28	6.00
OP 11	11	38.088932	-122.146535	191.32	6.00
OP 12	12	38.088835	-122.146262	189.79	6.00
OP 13	13	38.088733	-122.146037	187.96	6.00
OP 14	14	38.088641	-122.145629	188.97	6.00
OP 15	15	38.088691	-122.145345	190.06	6.00
OP 16	16	38.088522	-122.145076	189.01	6.00
OP 17	17	38.088964	-122.149402	220.54	6.00
OP 18	18	38.088617	-122.151312	249.51	6.00
OP 19	19	38.087342	-122.155356	248.27	6.00
20-ATCT	20	38.265538	-121.933272	51.83	100.00

Map image of 20-ATCT



ForgeSolar Glare Analysis Report (Sunset Backtrack Simulation) – Page 7 of 13

Route Receptor(s)

Name: Route 1 Path type: Two-way Observer view angle: 50.0°



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	38.098603	-122.156958	147.86	3.50	151.36
2	38.098464	-122.154163	151.17	3.50	154.67
3	38.098411	-122.152891	146.38	3.50	149.88
4	38.098283	-122.152460	145.63	3.50	149.13
5	38.097681	-122.151210	127.57	3.50	131.07
6	38.097535	-122.150708	114.88	3.50	118.38
7	38.097267	-122.148975	103.07	3.50	106.57
8	38.097105	-122.148418	117.17	3.50	120.67
9	38.096507	-122.146875	85.81	3.50	89.31
10	38.095543	-122.145159	100.36	3.50	103.86
11	38.095207	-122.144547	120.38	3.50	123.88
12	38.095026	-122.144196	127.21	3.50	130.71
13	38.094924	-122.143858	131.01	3.50	134.51
14	38.094922	-122.143316	134.99	3.50	138.49
15	38.095232	-122.140725	137.78	3.50	141.28
16	38.095517	-122.138239	136.33	3.50	139.83
17	38.095431	-122.137447	148.37	3.50	151.87
18	38.095277	-122.137005	148.82	3.50	152.32
19	38.095045	-122.136624	145.33	3.50	148.83
20	38.094711	-122.136243	139.69	3.50	143.19
21	38.093616	-122.134698	130.76	3.50	134.26
22	38.092566	-122.132939	153.79	3.50	157.29
23	38.091918	-122.131833	176.45	3.50	179.95
24	38.091621	-122.130903	182.10	3.50	185.60
25	38.091015	-122.128041	180.03	3.50	183.53
26	38.090618	-122.125619	197.60	3.50	201.10

GLARE ANALYSIS RESULTS

Summary of Glare

PV Array Name	Tilt	Orient	"Green" Glare	"Yellow" Glare	Energy
	(°)	(°)	min	min	kWh
PV array	30.0	270.0	122	10,281	9,190,000.0

Total annual glare received by each receptor

Receptor	Annual Green Glare (min)	Annual Yellow Glare (min)	
Runway 03L	0	0	
Runway 03R	0	0	
Runway 212 (assault strip)	0	0	
Runway 21L	0	0	
Runway 21R	0	0	
Runway 32 (assault strip)	0	0	
OP 1	98	8474	
OP 2	0	1807	
OP 3	0	0	
OP 4	0	0	
OP 5	0	0	
OP 6	0	0	
OP 7	0	0	
OP 8	0	0	
OP 9	0	0	
OP 10	0	0	
OP 11	0	0	
OP 12	0	0	
OP 13	0	0	
OP 14	0	0	
OP 15	0	0	
OP 16	0	0	
OP 17	0	0	
OP 18	0	0	
OP 19	0	0	
20-ATCT	0	0	
Route 1	24	0	

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Receptor	Green Glare (min)	Yellow Glare (min)	
Runway 03L	0	0	
Runway 03R	0	0	
Runway 212 (assault strip)	0	0	
Runway 21L	0	0	
Runway 21R	0	0	
Runway 32 (assault strip)	0	0	
OP 1	98	8474	
OP 2	0	1807	
OP 3	0	0	
OP 4	0	0	
OP 5	0	0	
OP 6	0	0	
OP 7	0	0	
OP 8	0	0	
OP 9	0	0	
OP 10	0	0	
OP 11	0	0	
OP 12	0	0	
OP 13	0	0	
OP 14	0	0	
OP 15	0	0	
OP 16	0	0	
OP 17	0	0	
OP 18	0	0	
OP 19	0	0	
20-ATCT	0	0	
Boute 1	24	0	

Results for: PV array

Flight Path: Runway 03L

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 03R

0 minutes of yellow glare 0 minutes of green glare

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Flight Path: Runway 212 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21L

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 21R

0 minutes of yellow glare 0 minutes of green glare

Flight Path: Runway 32 (assault strip)

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 1

8474 minutes of yellow glare 98 minutes of green glare





Point Receptor: OP 2

1807 minutes of yellow glare 0 minutes of green glare

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Point Receptor: OP 3

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 4

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 5

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 6

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 7

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 8

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 9

0 minutes of yellow glare 0 minutes of green glare

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Point Receptor: OP 10

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 11

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 12

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 13

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 14

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 15

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 16

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 17

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 18

0 minutes of yellow glare 0 minutes of green glare

Point Receptor: OP 19

0 minutes of yellow glare

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Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.

Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.

The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.

The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual results and glare occurrence may differ.

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

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Appendix D: Thomas Cleveland's CV

Thomas (Tommy) H. Cleveland, P.E.

4141 Laurel Hills Rd. Raleigh, NC	thcleveland@gmail.com	919-923-5490
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Education & Training

North Carolina State University, Mechanical Engineering M.S. 2004 North Carolina State University, Mechanical Engineering B.S., Business Mgmt. minor 2001 - Summa Cum Laude Lumberton Sr. High School, Lumberton, NC, 1997 – Valedictorian

Professional Engineer, licensed in North Carolina (#033711), 2008 - Present

Professional Experience

Solar PV Engineer, Advanced Energy, Raleigh, NC, April 2017–Present

- Evaluation of commercial and utility scale solar PV facilities to assess the quality of design, construction, and operation
- Engineering analysis and concise presentation of results to customers

Solar Energy Engineer (various progressive titles), North Carolina Solar Center/NC Clean Energy Technology Center, North Carolina State University, 2005–April, 2017

- Lead solar engineer at the Center (2008-2017)
- Conducted detailed PV + storage feasibility study for community solar project for a NC municipal utility
- Provided quality assurance and technical support to development of in-house training program of every stage of solar farm construction for a leading regional utility-scale photovoltaic EPC firm
- Guided design of prototype residential Plug and Play PV system and collected AHJ feedback (Department of Energy SunShot project)
- Co-led stakeholder process to develop Template Solar Development Ordinance for North Carolina
- Led design and development of ISO-17025 accredited solar thermal collector testing lab
- Designed and installed PV field performance monitoring system, conducted performance analysis
- Conducted renewable energy site assessments for commercial, industrial, and institutional clients
- Presented to local government officials, community leaders, and general public on solar energy
- Provided technical support to a wide variety of energy consumers and stakeholders across North Carolina

Consultant/Expert Witness, Private consultant for over 15 solar developer clients, 2012-Present

- Provides expert witness testimony at special/conditional use and re-zoning public hearings regarding the health, safety, and environmental impact of utility-scale solar photovoltaic systems. Experience in NC, SC, VA, and FL (over 60 projects to date)
- Provides respectful clear answers to sometimes ill-informed and/or hostile questions
- Conduct site-specific studies of EMF, sound, and solar glare hazard for several projects

Instructor of ET 220 Solar Photovoltaic Assessment, Department of Forestry and Environmental Resources, North Carolina State University, 2014-Present

- Developed all course content for this new three credit hour online course
- Course covers all aspects of photovoltaic site assessment including energy use, solar resource, system design, utility tariffs, estimating, economics, and more
- Course is optional course for an Environmental Technology and Management degree
- Course is required for a Renewable Energy Assessment minor

Instructor of MAE 421 Design of Solar Energy Systems, Mechanical and Aerospace Engineering Department of North Carolina State University, 2009-2014

- Instructor of the solar energy engineering course, MAE 421, in the NC State University Mechanical and Aerospace Engineering department
- The course was offered during the spring semester and typically had 30 to 50 undergraduate and up to twelve graduate engineering students
- Previously co-instructor of the course for two years (2007, 2009)

Research Assistant, North Carolina Solar Center, North Carolina State University, 2003–2005

- Developed and validated a TRNSYS simulation model of a unique solar thermal concentrating collector
- Assisted with the installation of photovoltaic systems ranging in capacity from 1 kW to 5 kW

Selected Publications

"Balancing Agricultural Productivity with Ground-Based Photovoltaic Development", NCCETC/NCSU white paper, August 2017, https://nccleantech.ncsu.edu/wp-content/uploads/Balancing-Ag-and-Solar-final-version-update.pdf

"Health and Safety Impacts of Photovoltaics", NCCETC/NCSU white paper, May 2017, https://nccleantech.ncsu.edu/wp-content/uploads/Health-and-Safety-Impacts-of-Solar-Photovoltaics-2017_white-paper-1.pdf

"Community Solar (+ Storage) Program Design for Fayetteville Public Works Commission", NCSU/NCCETC report, March 2017, (Public version) https://nccleantech.ncsu.edu/wpcontent/uploads/FPWC_CommunitySolar_Public_Version.pdf

T. Cleveland, H. Tsai, "Charlotte-Mecklenburg Schools Roadmap to 100% Renewable Electricity" & "Durham Public Schools Roadmap to 100% Renewable Electricity", NCCETC, February 2016

T. Cleveland, et al, "Template Solar Energy Development Ordinance for North Carolina", NCCETC & NCSEA, December 2013, www. go.ncsu.edu/template-solar-ordinance

M. Sheehan, T. Cleveland, "Updated Recommendations for Federal Energy Regulatory Commission Small Generator Interconnection Procedures Screens", Solar America Board for Codes and Standards Study Report, 64 p., July 2010, www.solarabcs.org/about/publications/reports/ferc-screens/pdfs/ABCS-FERC_studyreport.pdf

T. Cleveland, et al, "Optimizing Solar Thermal Resource Use at Commercial Buildings", Solar 2010 – ASES National Solar Energy Conference 2010, 6 p., May 2010, www.ases.org/papers/101.pdf

T. Cleveland, "Description and Performance of a TRNSYS Model of the Solargenix Tracking Power $Roof_{TM}$ ", Solar 2005 – ASES National Solar Energy Conference, 6 p.

T. Cleveland, K. Creamer, & Dr. R. Johnson, *"Energy Metering of Solar Domestic Hot Water Systems for Inclusion in Green Power and Renewable Portfolio Standards Programs"*, Solar 2004 – ASES National Solar Energy Conference 2004, 6 p.

T. Cleveland, "Effective Energy Metering of Solar Domestic Hot Water Systems for Inclusion in Green Power and Renewable Portfolio Standards", Master's Thesis, North Carolina State University, Raleigh, 191 p., April 2004, http://repository.lib.ncsu.edu/ir/handle/1840.16/1152

Selected Recent Presentations

T. Cleveland, A. Huang, "Plug and Play Residential PV System Innovation and Demonstration", Solar Power International Conference 2015

T. Cleveland, "Make Solar Energy Economical", recorded video lecture for E102: Grand Challenges of Engineering course at NC State University, January 2015

T. Cleveland, M. Clark, "Template Solar Ordinance for North Carolina", Solar Power International Conference 2014

Coblentz Patch Duffy & Bass LLP

One Montgomery Street, Suite 3000 San Francisco, CA 94104 T 415 391 4800 700 Main Street, Suite 210 Napa, CA 94559 T 707 603 2722 coblentzlaw.com

Jeff Dodd D (415) 772-5724 jdodd@coblentzlaw.com

July 30, 2019

VIA ELECTRONIC MAIL (email: aaron@renewprop.com)

Aaron Halimi RPCA Solar 4, LLC 655 Montgomery Ave., Suite 1430 San Francisco, CA 94111

Re: Benicia zoning text amendment

Dear Aaron:

This letter provides additional guidance on a zoning text amendment to facilitate a solar utility project ("Project") in the City of Benicia, North of Lake Herman Road (APN: 080-030-050; the "Property"). As you know, the Property is within the "OS – Open Space" zoning district. The uses within the "OS – Open Space" district are set forth in Chapter 17.36 of the Benicia Municipal Code (BMC).

As noted in our May 30, 2019 letter to you, the Project can amend the BMC to create and define a new land use classification of "Utilities, Solar" and permit that use in the "OS" zoning district, subject to a conditional use permit. Based on input from the Community Development Department, the Project should also amend Chapter 17.70 to address the conditions for developing a solar utility project in the City. The Project's compliance with these conditions would measure how the City would issue a conditional use permit for a solar utility use.

We have provided the proposed zoning text amendments to both BMC Chapters 17.36 and 17.70 to facilitate the Project below. All amendments are identified in red font.

I. <u>Amendments to Chapter 17.36 (OS OPEN SPACE DISTRICT)</u>

BMC § 17.16.040 Public and semipublic use classifications.

"*Utilities, solar*" means photovoltaic electric panels and appurtenant structures and facilities, designed to provide energy for off-site use such as a power purchase agreement, or direct sale of energy to a local utility company.

BMC § 17.36.030 Land use regulations.

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Aaron Halimi July 30, 2019 Page 2

OS District: Land Use Regulations

	OS	Additional Regulations
Public and Semipublic		
Utilities, Major	U	(F)
Waste Facility	U	(F)
Utilities, Solar	U	(1)
Utilities, Minor	Р	

OS District: Additional Use Regulations [footnotes for L1 – H omitted]

(I) See BMC 17.70.420, Solar utilities.

II. Amendments to Chapter 17.70 (GENERAL REGULATIONS)

BMC § 17.70.420 Solar utilities.

The following standards shall apply to all solar utilities:

- A. Agricultural Protections. Solar utilities shall not be sited on any land subject to a Williamson Act Contract, unless the landowner has rescinded that contract pursuant to its terms.
- B. No Municipal Services. Solar utilities shall not require or benefit from municipal services, such as water or sewer services.
- C. Development Standards. Solar arrays shall comply with all applicable setback restrictions, including creek setbacks, for the applicable zoning district.
- D. Height. For ground-mounted installations, the maximum height shall not exceed 15 feet from finished grade.
- E. Noise. Noise levels shall be in compliance with the noise regulations identified in Chapter 8.20 BMC.
- F. Decommissioning. Upon ceasing operations, or if the facility is non-operational for a period of 12 months, the facility should be decommissioned (or deactivated and removed) in an efficient and thorough manner.

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Aaron Halimi July 30, 2019 Page 3

- G. Stormwater Management. All projects greater than one acre shall submit a Stormwater Pollution Prevention Plan and include erosion and sediment control best management practices into the plan.
- H. Minimal Traffic. Solar utilities shall not generate new daily traffic trips during normal operation outside of occasional trips for maintenance.

We believe the proposed amendments to BMC Chapters 17.36 and 17.70 address the City's request for providing the appropriate conditions under which the City could issue a conditional use permit for the development of a solar utility, including the Project. We would be happy to discuss this further with the City Attorney or the Community Development Department upon your request.

Sincerely yours,

COBLENTZ PATCH DUFFY & BASS LLP

Jeff Dodd

jtd:JTD
Travis AFB Context Map



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